

APPLICATION OF RESINOUS BINDERS WITH INCORPORATION OF CARBONATED SLUDGES FROM THE DIMENSION STONE INDUSTRY IN THE PRODUCTION OF STONE COMPOSITES

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INTRODUCTION

The carbonated dimension stone extractive and processing industry produce high amounts of wastes that are deposited in the open in heaps and deposits of carbonated sludge (Fig. 1). The industrial application of this waste makes it possible to add value, transforming it into a by-product, thus contributing to the framing of the limestone and marble extractive and processing sub-sectors, in the “Action Plan for the Circular Economy”, promoting the sustainable growth. By this means, this research has shown that the recycling slurries as a raw material are possible to integrate binders production through its incorporation on the manufacture of ornamental stone composite materials, partial or totally replacing the epoxy resins traditionally used in this type of products.

RESULTS & DISCUSSION

Sludges - Chemical Characterization

The chemical analyses (Table 1) carried out using atomic spectrometry revealed a fundamentally carbonated material. All carbonated sludges have significant percentages of CaO and show relevant percentage of loss of ignition.

Formulation of Binders Consisting of Carbonated Sludge and Resin

Table 2: Results of uniaxial compressive strength tests after 28 days of curing.

Formulations %	R (MPa)
ANM3 – 54,43%NM / 45,57%Res.	102.73
ANM4 – 50%NM / 50%Res.	98.35
ANM5 – 47%NM / 53%Res.	96.23
ANM6 – 52%NM / 48%Res.	106.37
ANC3 – 52,31%NC / 47,69%Res.	103.20
ANC4 – 50%NC / 50%Res.	102.12
ANC5 – 47%NC / 53%Res.	96.04

NM – Marble sludge; NC – Limestone sludge; Res – Resin.

The mechanical characterization of the binder was carried out by evaluating the resistance to uniaxial compression of the different formulations with different percentage contributions of limestone and marble sludge and resin. The specimens kept for curing in air and were tested at 7, 14 and 28 days, with increasing uniaxial compressive strength over this period, reaching higher uniaxial compression values at 28 days (Table 2).

Composite Formulations with Binder 52/48 and Marble Aggregates

Having defined the formulations with the best performance, in terms of uniaxial compressive strength tests (NP EN 1926-2008) (Table 3), the remaining characterization tests were made, namely:

- determination of flexural strength under concentrated load;
- apparent density and porosity (NP EN 1936-2008);
- absorption of water at atmospheric pressure (NP EN 13755);
- absorption of water by capillarity (NP EN 1925-2000).

Table 4: Characterization tests for the binders.

Curing (Days)	Binder	i				ii			iii		iv	
		Flexural strength (MPa)	Open pore Volume (ml)	Apparent volume (ml)	Apparent density (g/m ³)	Open porosity (%)	Water absorption at atmospheric pressure (%)	Average (g/m ² s)				
28	Marble	1549 ± 1.38	0.22 ± 0.03	117.0 ± 7.0	2.279 ± 0.014	0.19 ± 0.02	0.2 ± 0.03	0.088 ± 0.010				
	Limestone	13,49 ± 0.97	0.21 ± 0.04	104.6 ± 7.4	2.263 ± 0.017	0.20 ± 0.03	0.1 ± 0.03	0.062 ± 0.019				

Table 3: Stone composite formulations and uniaxial compressive strength test results for the several formulations.

Formul.	Aggregates			Binders		Average uniaxial Compression Strength (MPa)
	BA	B1	B2	NC	NM	
F1	30%	30%	40%	52%	48%	73.30
F2	20%	20%	60%	52%	48%	69.06
F3	35%	15%	50%	52%	48%	61.11
F4	40%	40%	20%	52%	48%	91.96
F5	30%	30%	40%	52%	48%	52.26
F6	20%	20%	60%	52%	48%	76.33
F7	35%	15%	50%	52%	48%	81.20
F8	40%	40%	20%	52%	48%	88.19

The marble aggregate, supplied by the company *Marvisa, Mármores Alentejanos Lda.*, consisted of three types, with the following granulometric intervals: BA (4 mm / 6.3 mm), B1 (8 mm / 14 mm) and B2 (14 mm / 25 mm) (Table 3).

CONCLUSIONS

The use of polyester resin in replacement of epoxy resin seems feasible. The price of epoxy resin is on average four times higher than polyester resin, which makes stone composite products substantially more expensive.

As one goal of the investigation was the reduction of resin and its partial replacement by carbonated sludge, the investigation gradually incorporated successively higher percentages of solid load, without compromising the strength of the specimens. Thus, the ideal binder percentage was: 52% carbonated sludge and 48% polyester resin.

The results obtained in the compressive and flexural strength tests are promising, given the fact that the formulations were carried out manually using a manual mixer.



ACKNOWLEDGMENTS

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Fig. 1. Deposit of carbonated sludge in the factory *Criamármore - Mármores Portuguesas, Lda*

MATERIALS

The slurries were sampled in the filter presses plants at the companies: António Galego & Filhos – Mármores SA, referred to as M(AGF) and A.L.A. de Almeida SA, referred to as M(A). The limestone carbonated sludge was collected at Solancis - Sociedade Exploradora de Pedreiras SA, referenced as C(S) and MVC - Mármores de Alcobaca Lda., referenced as C(MVC).

NEW RESULTS

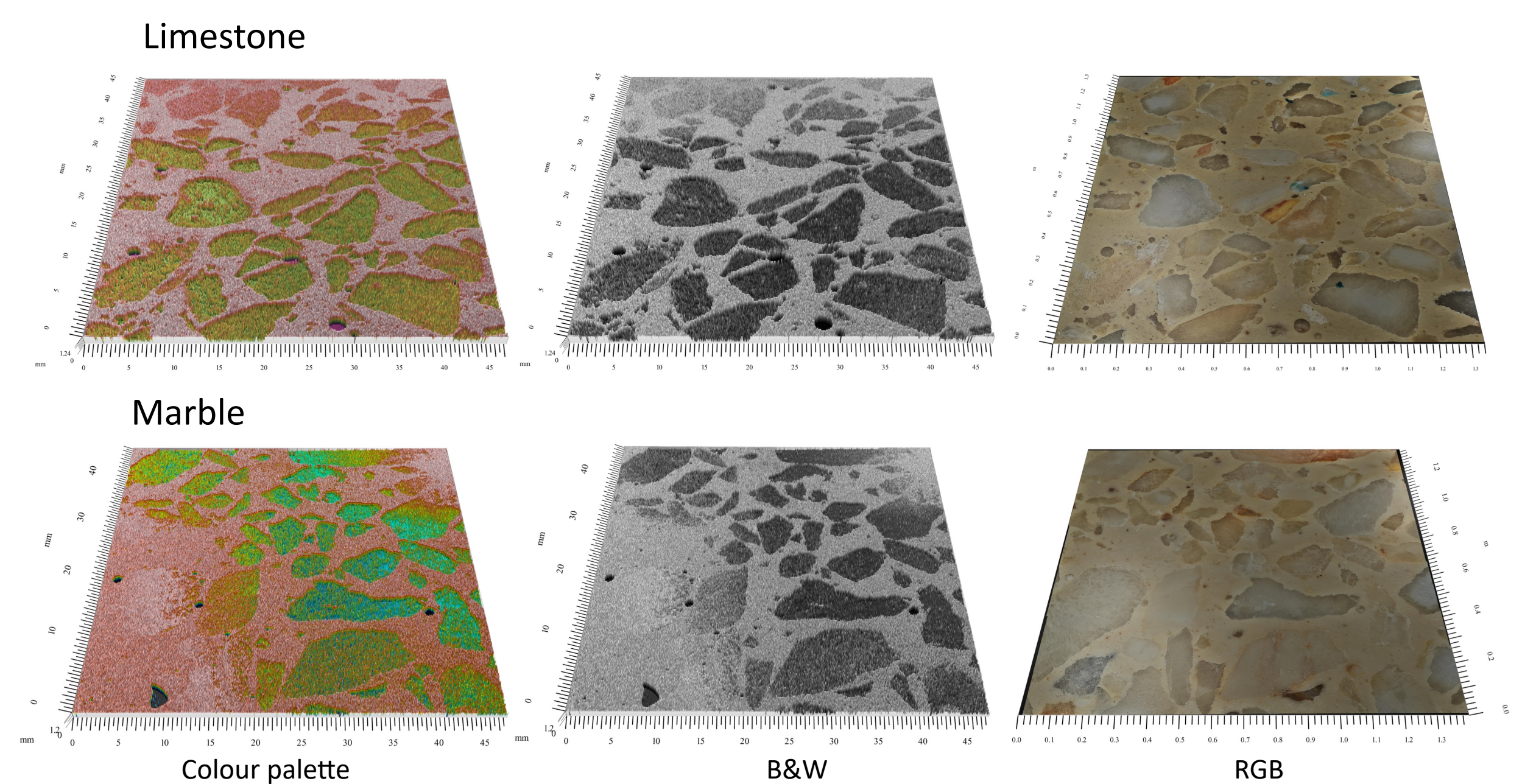


Fig. 2. Micro-topographic maps of limestone and marble sludge binder.

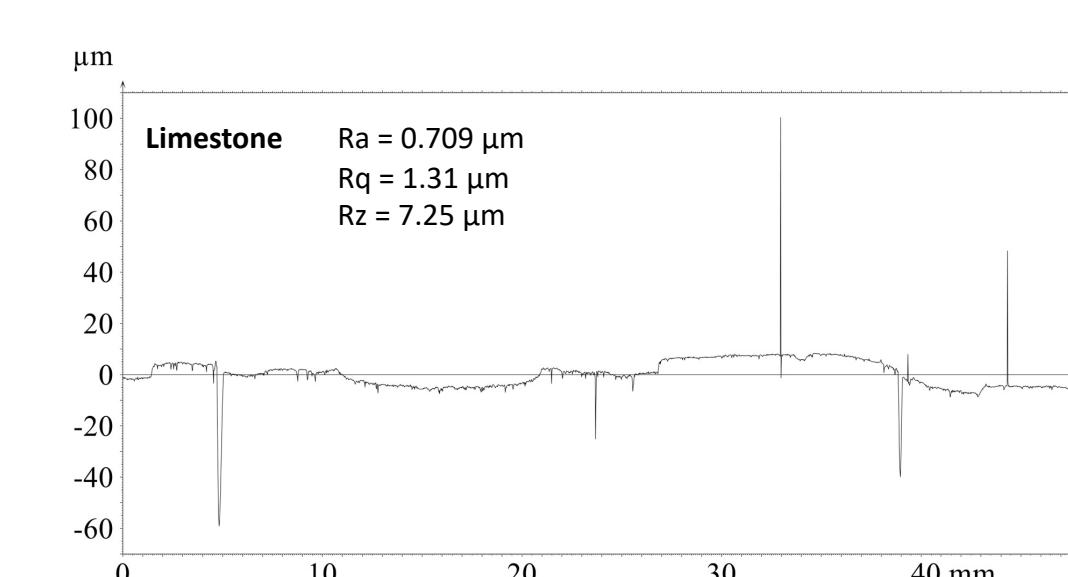


Fig. 3. Roughness profile of limestone sludge binder.

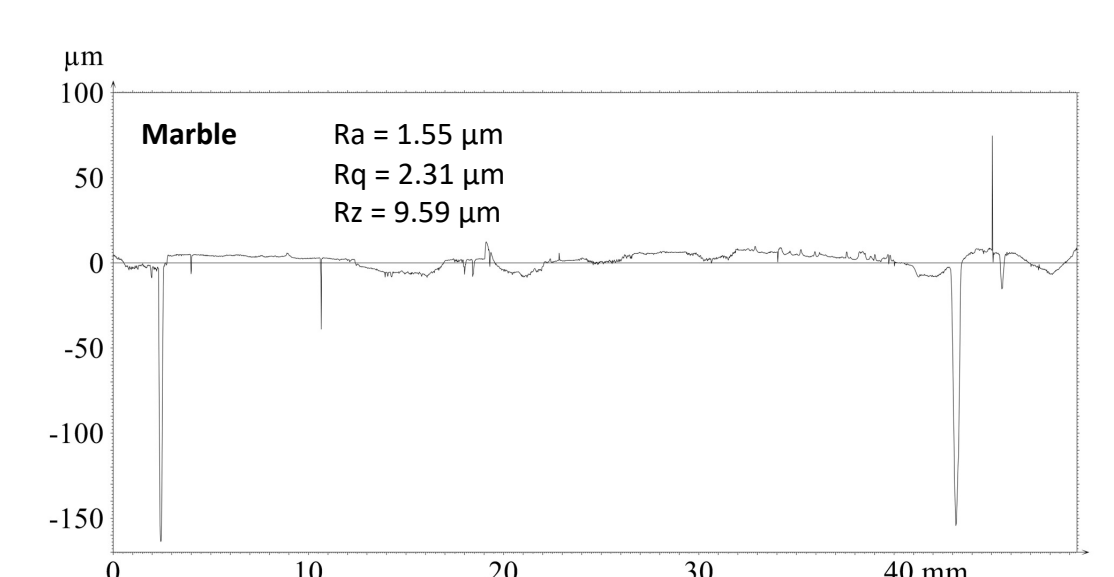


Fig. 4. Roughness profile of marble sludge binder.

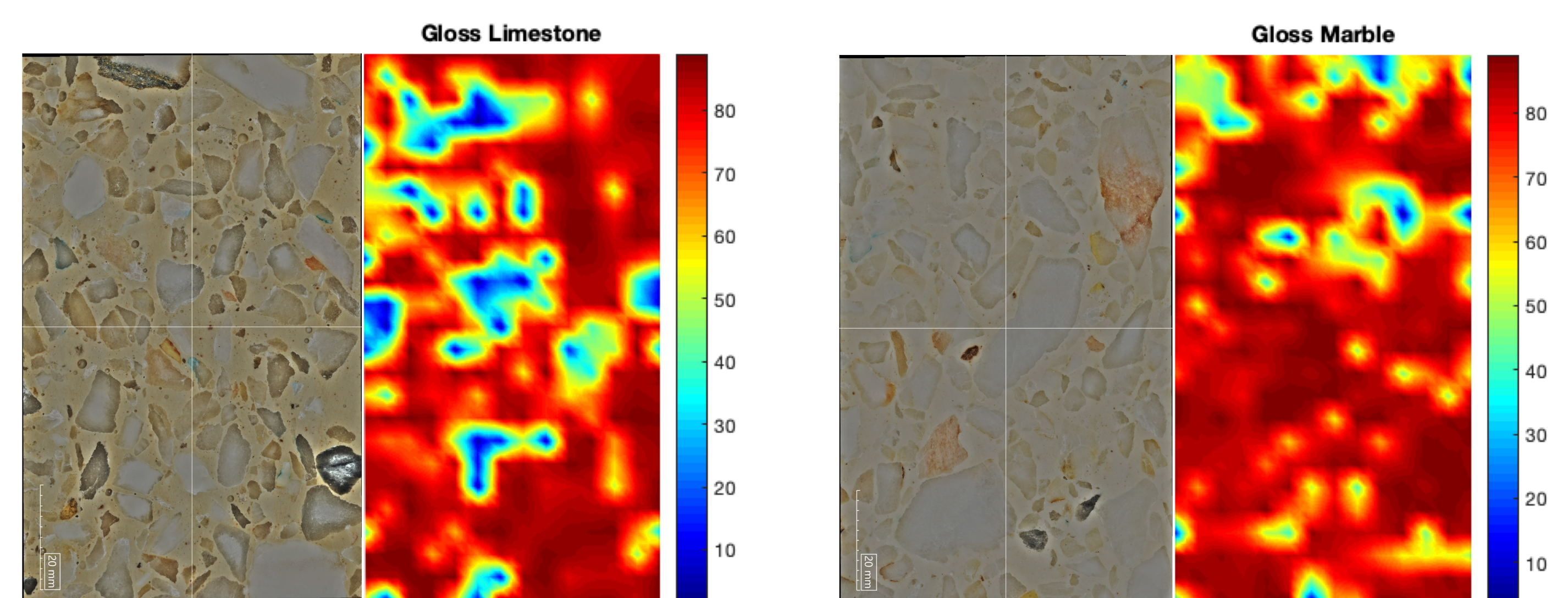
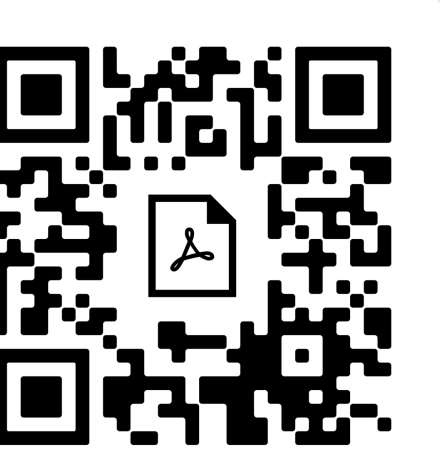


Fig. 5. Gloss maps on polished surfaces of limestone sludge binder.

Fig. 6. Gloss maps on polished surfaces of marble sludge binder.



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